

## Ballasted System Attachment

For a Non penetrating application we suggest using 1/2" sch40 galvanized pipes, glued across the width of the solar mat at 4-5 foot intervals.





# **INLAND ENGINEERING & CONSULTING, INC.**

Structural & Civil Engineering

4883 EAST LA PALMA AVENUE - SUITE 501-A  
ANAHEIM, CA 92807  
Tel.: (714) 777-7700  
FAX: (714) 777-7773

SHT. # 1 OF 8

JOB # 81348

DATE: 8-8-08

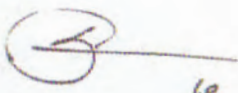
## **STRUCTURAL CALCULATIONS**

PREPARED FOR:

SUN TREK

PROJECT:

SOLAR POOL HEATING ATTACHMENT  
WOODSIDE HIGH SCHOOL  
199 CHURCHILL AVE.  
WOODSIDE, CA. 94062



8-12-08



**INLAND ENGINEERING**

DATE \_\_\_\_\_

SUBJECT

WOODSIDE H.S.

SHEET NO.

2

BY \_\_\_\_\_

CHKD. \_\_\_\_\_

JOB NO.

81348

GENERAL INFORMATION:BUILDING CODE: 2007 CBCMATERIAL PROPERTIESLUMBER: (STRUC. LUMBER DOUGLAS FIR LARCH)

	GRADE	Fb	Ft	Fv	E	Fc
2x AND 4x JOIST AND BEAM.....	No. 2	875	575	95	$1.6 \times 10^6$	1300
	No. 1	1000	575	95	$1.7 \times 10^6$	1300
	SELECT	1450	575	95	$1.9 \times 10^6$	1300
6x BEAMS & THICKER.....	No. 1	1350	675	85	$1.6 \times 10^6$	925
6x POSTS.....	No. 1	1350	825	85	$1.6 \times 10^6$	1000
GLU-LAMINATED BEAMS.....	24-F-V4	2400	1100	165	$1.8 \times 10^6$	1600
PSL-PARALLAM OR EQ. ....		2800	1850	285	$2.0 \times 10^6$	2700

<u>CONC.:</u>	fc	wt.
SLAB ON GRADE.....	2500 psi	150pcf
FOOTING.....	2500 psi	150pcf

MASONRY:

CONC. BLOCK.....1500 psi

REINF. STEEL: .....# 4 BAR AND SMALLER GR. 40.  
# 5 BAR AND LARGER GR. 60.

STRUC STEEL:

STRUC. PLATES.....Fy = 36 ksi  
PIPE COLS.....Fy = 35 ksi  
STL. TUBES.....Fy = 46 ksi

# INLAND ENGINEERING

DATE \_\_\_\_\_

SUBJECT WOODSIDE H.S.

SHEET NO. 3

BY \_\_\_\_\_

CHKD. \_\_\_\_\_

JOB NO. 81348

## SCOPE OF WORK:

SUNTREK'S SOLAR SYSTEM ATTACHMENT ON FLAT ROOF:

WT. OF SYSTEM : 1.5 PSF FULL

MAX. COLLECTOR SPAN = 70 FT.

## DESIGN LOADS:

### WIND LOAD

85 MPH EXP. "C"

ASSUMED HT. OF ROOF : 20 FT.

$$K_z = .90$$

$$K_{zt} = 1.0$$

$$K_d = .85$$

$$I = 1.0$$

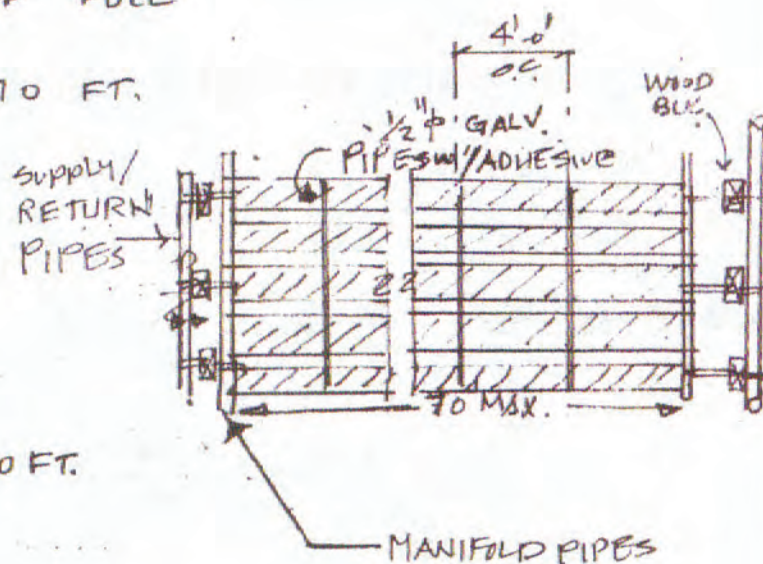
$$q_h = .00256 (K_z)(K_{zt})(K_d) V^2 I$$

$$= .00256 (.9)(1.0)(.85)(85)^2 (1.0) = 14.15 \text{ PSF}$$

NEG. EXTERNAL PRESSURE COEFF. FOR  $(GCP) = -.9$

$$P_w = q_h [GCP - GCP_i]$$

$$P_w = 14.15 [-.9 - .18] = 15.3 \text{ PSF}$$





# INLAND ENGINEERING

DATE \_\_\_\_\_ SUBJECT WOODSIDE H.S. SHEET NO. 4  
 BY \_\_\_\_\_ CHKD. \_\_\_\_\_ JOB NO. 81348

SEIS. LOAD:

$$F_p = \frac{.4 a_p S D S W P}{(R_p / I_p)} \left( 1 + 2 \frac{z}{h} \right) \begin{cases} < F_p = 1.6 S D S F_p W P \\ > .3 S D S F_p W P \end{cases}$$

$$a_p = 2.5, R_p = 3.0, I_p = 1.0 \quad S D S = 2/3 S M S$$

$$S M S = F_a S_s \quad F_a = 1.0 \quad F_v = 1.5 \quad S_s = 2.251, S_1 = 1.087$$

$$S M S = (1.0)(2.251) = 2.251$$

$$S D S = 2/3 (2.251) = 1.50 \quad \left. \begin{array}{l} \\ \end{array} \right\} \text{SITE CLASS "D"} \quad \text{ZIP CODE: 94062}$$

$$F_p = \frac{(.40)(2.5)(1.5) W P}{(3. / 1)} \left( 1 + 2 \frac{20}{20} \right) = 1.5 W$$

$$F_{p \max} = 1.6 (1.5) (1.0)(W P) = 2.4 W P$$

$$F_{p \min} = .3 (1.5) (1.0)(W P) = .45 W P \quad \left. \begin{array}{l} \\ \end{array} \right\} \text{OK}$$

NOTE: \* COLLECTORS ARE 2'-0" WIDE

\* COLLECTORS ARE ATTACHED TO R.F. @ 4'-0" O.C.  
 W/ 1/2" GALV. PIPES GLUED W/ SONTREK ADHESIVE

$$T.A. \text{ of COLLECTORS} = 4' \times 4' = 16 \text{ SF.}$$

$$L.W.T. = 1.5 \text{ PSF} (16') = 24 \text{ LB/FT.}$$

WIND LOAD:  $F_{W} = 15.3 \text{ PSF} (16') = 245 \text{ LB/FT.}$

SEIS. LOAD:  $F_S = 1.5 (24) = 36 \text{ LB/FT.}$

# INLAND ENGINEERING

DATE _____	SUBJECT <u>WOODSIDE H.S.</u>	SHEET NO. <u>5</u>
BY _____	CHKD. _____	JOB NO. <u>81 348</u>

## ADHESIVE STRENGTH (SUNTREK SEALANT)

BASED ON TEST RESULTS PROVIDED BELOW :

AVERAGE TENSILE STRENGTH IS GIVEN AS  $8.04 \frac{\text{#}}{\text{IN}}$

$$F_t = 48" (8.04) = 386 \text{#} > 245 \text{#} \quad F.S. = 1.5$$

The following table is a summary of the data collected during our testing:

Substrates (Adherents)	Average Peel Strength (Pounds Per Linear Inch)
Suntrek Rubber Tubing / Ceramic Tile	12.156
Suntrek Rubber Tubing / Composition Roofing	10.996
Suntrek Rubber Tubing / Wood (maple)	8.045

## PHYSICALS OF SUNTREK SOLAR TUBE

SAMPLE	SLAB-DUMBBELL	TUBE
DURO, A	80	80
TENSILE STRENGTH, psi	1728	1479
ELONGATION, %	247	224
MOD@25%, psi	355	281
MOD@50%, psi	370	473
MOD@75%, psi	807	686
MOD@100%, psi	1001	899
MOD@200%, psi	1582	1448



# INLAND ENGINEERING

DATE \_\_\_\_\_

SUBJECT WOODSIDE H.S.

SHEET NO. 6

BY \_\_\_\_\_

CHKD. \_\_\_\_\_

JOB NO. 81378

## CONNECTION OF 2" $\phi$ MANIFOLD

2"  $\phi$  PVC MANIFOLD ATTACHED TO WOOD BLKS

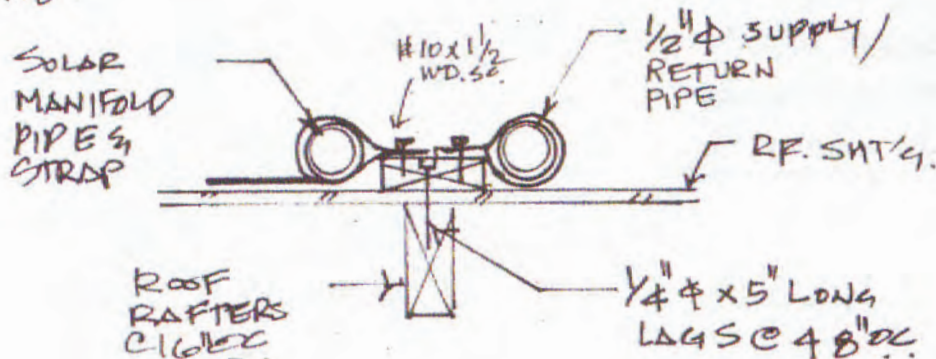
@ 32" O.C. • WOOD BLKS ARE LAGED INTO ROOF RAFTERS

W/ 1/4"  $\phi$  x 5" LAGS @ 32" O.C. (TYP. END CONDITION)

ALSO 1/2"  $\phi$  GALV. SCH. 40 PIPES PROVIDED @ 4' O.C.

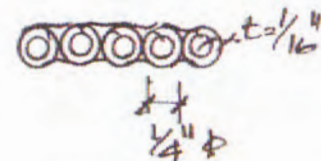
ACROSS THE SOLAR PANELS W/ SUNTREK BOND

ADHESIVE.



SOLAR PANEL TIES (STRAPS) CONSISTS OF 1/4"  $\phi$  PLASTIC TUBING (TOTAL OF 5 - 1/4"  $\phi$  TUBING)

ALLOW. TENSILE STRENGTH = 1479 PSI



$$A = \pi D^2 / 4 = \frac{\pi (.125^2 - .125^2)}{4} = .036 \text{ IN}^2$$

$$\Sigma A = 5 (.036) = .184 \text{ IN}^2$$

$$T_{\text{ALLOW.}} = 1479 \text{ PSI} (.184) = 272 \text{ \#}$$

# INLAND ENGINEERING

DATE \_\_\_\_\_

SUBJECT WOODSIDE H.S.

SHEET NO. 7

BY \_\_\_\_\_

CHKD. \_\_\_\_\_

JOB NO. 81348

2"  $\phi$  PVC PIPE SCH. 40 FILLED W/ WATER

$$\Sigma WT. = (3.653 \frac{\#}{ft} + 1.453 \frac{\#}{ft}) \frac{48}{12} = 20.4 \frac{\#}{ft}$$

$$F_w = 4' \times 2 \times 15.3 = 122.4 \frac{\#}{ft} \leftarrow \text{CONTROLS}$$

$$F_s = 20.4 \times 1.5 = 31 \frac{\#}{ft}$$

1/4"  $\phi$  LAG SC. INTO WOOD RAFTERS W/ 2" MIN. EMB.

$$TALL = 225 \frac{\#}{IN} (2") = 450 \frac{\#}{ft} > 122.4 \frac{\#}{ft} \text{ OK}$$

USE: 4 X 12" WOOD BLOCK  
W/ 1/4"  $\phi$  WD. SC.  
2" MIN. EMB. INTO  
ROOF RAFTERS  
@ MAX. 2' LAG SC.



# INLAND ENGINEERING

DATE \_\_\_\_\_

SUBJECT

WOODSIDE H.S.

SHEET NO.

8

BY \_\_\_\_\_

CHKD. \_\_\_\_\_

JOB NO.

81348

